

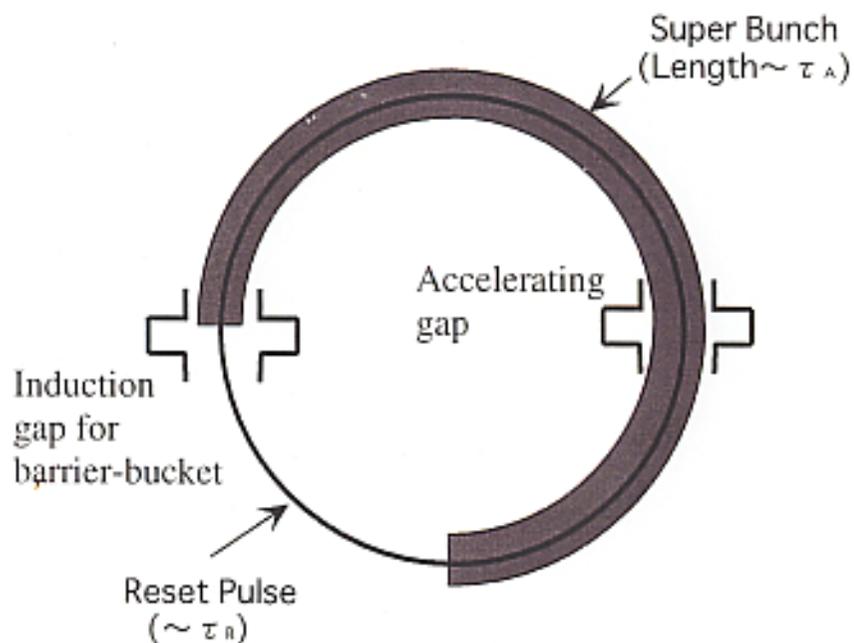
Magnetic Core Studies and
Beam Loading Effects
for Repetitive Induction Modulator

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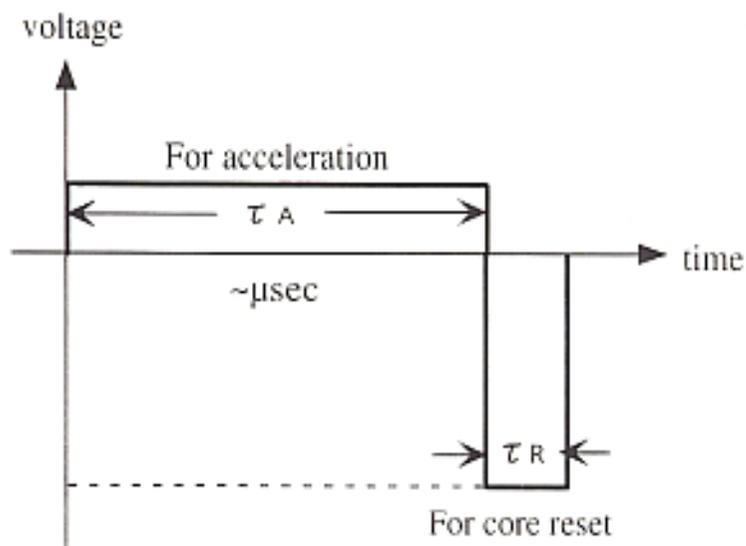
Schematic illustration of induction synchrotron and acceleration voltage waveform



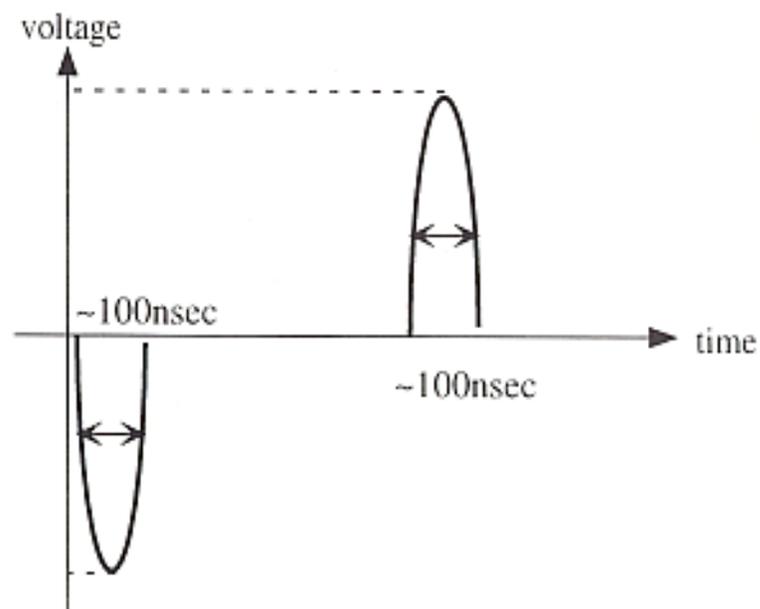
Induction Synchrotron

Induction modulator requires highly repetitive operation up-to \sim MHz.

Fast switching devices
Core-loss
Beam loading effect



Acceleration voltage waveform

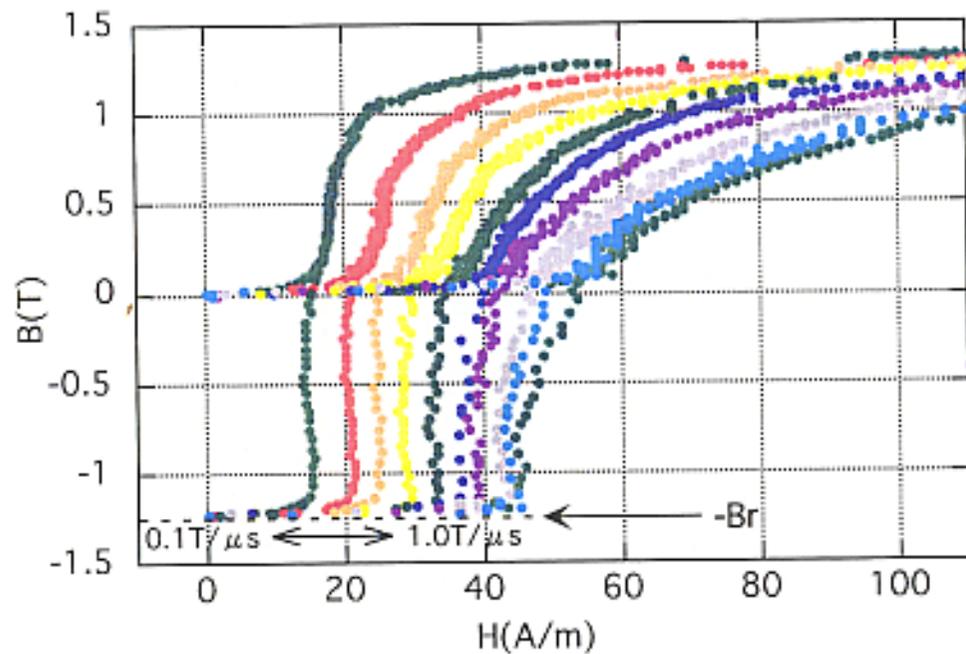


Barrier-bucket waveform

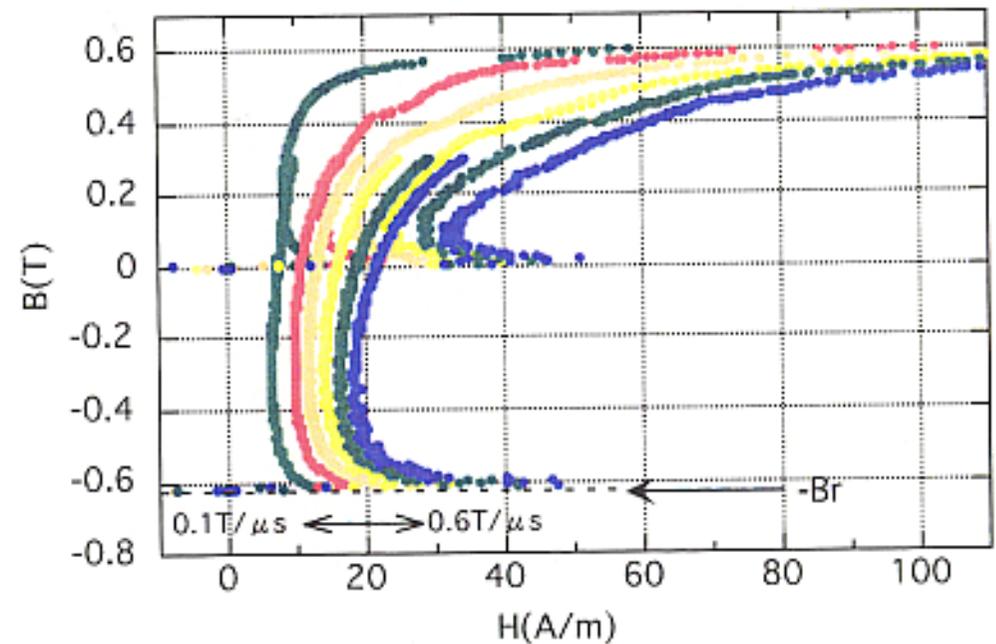
B-H curves from different magnetization state

Magnetization process depends on ΔB and dB/dt .

Finemet(FT-1H)



Co-amorphous (ACO-5H)



Core-loss depends on Magnetic Domain Motion

Saturation-wave mode

Bar-domain mode

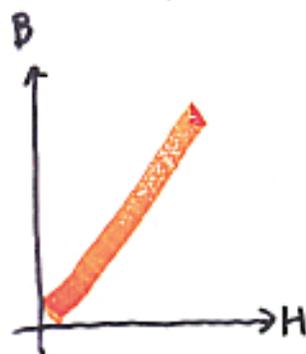
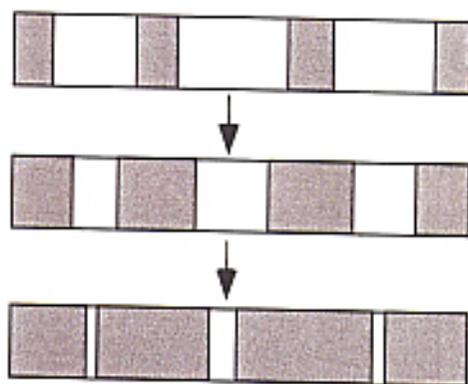
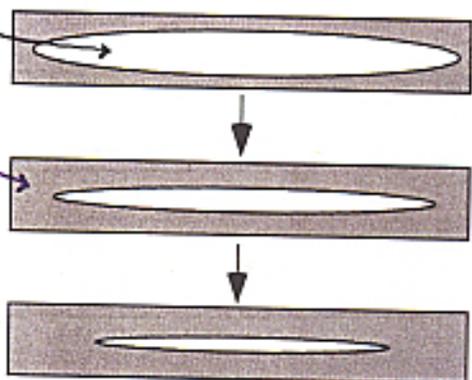
non-saturation region

saturation region

Magnetic field ⊙

Magnetization

Magnetic field ⊙

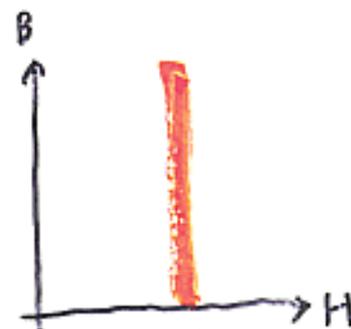


$$H_{SW} \propto \frac{d^2}{\rho} \left(\frac{\Delta B(t)}{2B_s} \right) \left(\frac{dB}{dt} \right)$$

$$P_{SW} (\text{J/m}^3) \propto \left(\frac{d^2}{\rho} \right) \left(\frac{(\Delta B)^2}{2B_s} \right) \left(\frac{dB}{dt} \right)$$

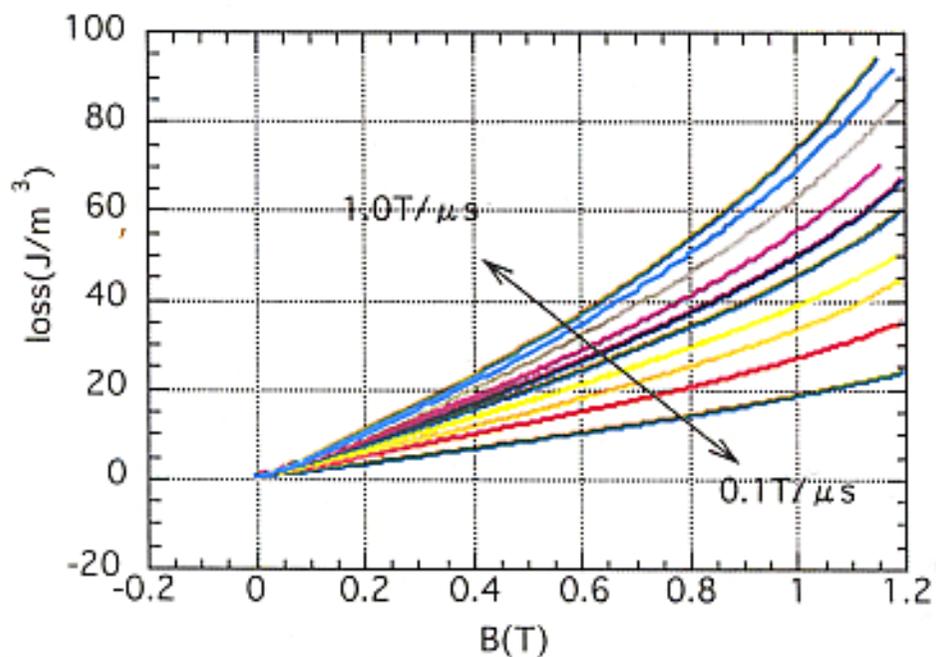
$$H_{BD} \propto \left(\frac{d}{\rho} \right) \sqrt{\left(\frac{dB}{dt} \right)}$$

$$P_{BD} (\text{J/m}^3) \propto \left(\frac{d(\Delta B)}{\rho} \right) \sqrt{\left(\frac{dB}{dt} \right)}$$

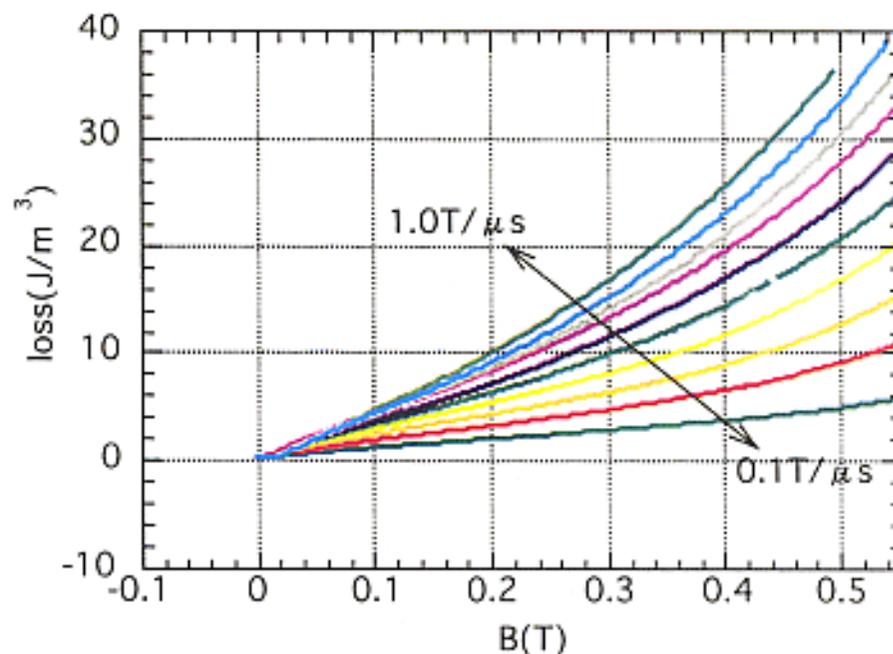


Core-loss scaling of Finemet(FT-1H) and Cobalt-based Amorphous(ACO-5H) versus flux swing(B)

Finemet(FT-1H)



Co-based amorphous (ACO-5H)



$$P\left(\frac{J}{m^3}\right) = \underbrace{C_1 \left(\frac{d}{\rho}\right) \left(\frac{dB}{dt}\right)^{1/2}}_{\text{(Bar-domain mode)}} + \underbrace{C_2 \left(\frac{d^2}{\rho B_s}\right) \left(\frac{dB}{dt}\right)}_{\text{(Saturation-wave mode)}}$$

Finemet

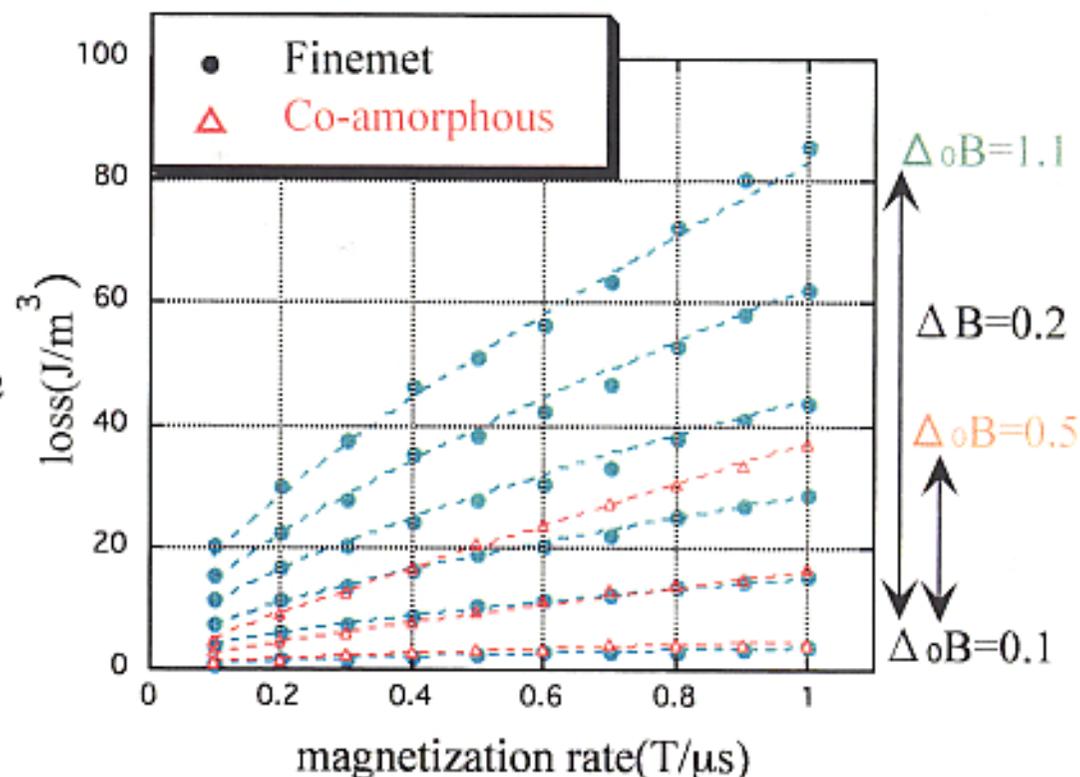
$$P(\Delta_0 B, dB/dt) = (-0.44 + 24.7 \Delta_0 B) (d/\rho) (dB/dt)^{1/2} + (10.6 \Delta_0 B^2) (d^2/\rho/B_s) (dB/dt),$$

Co-amorphous

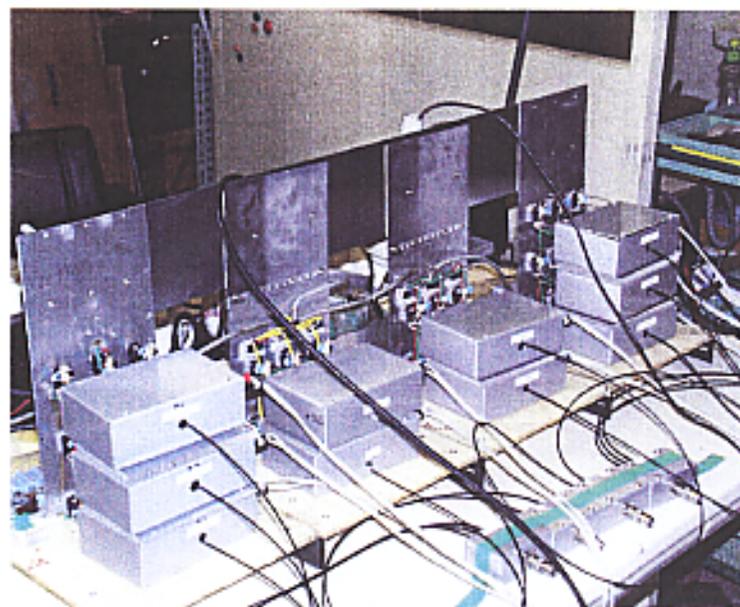
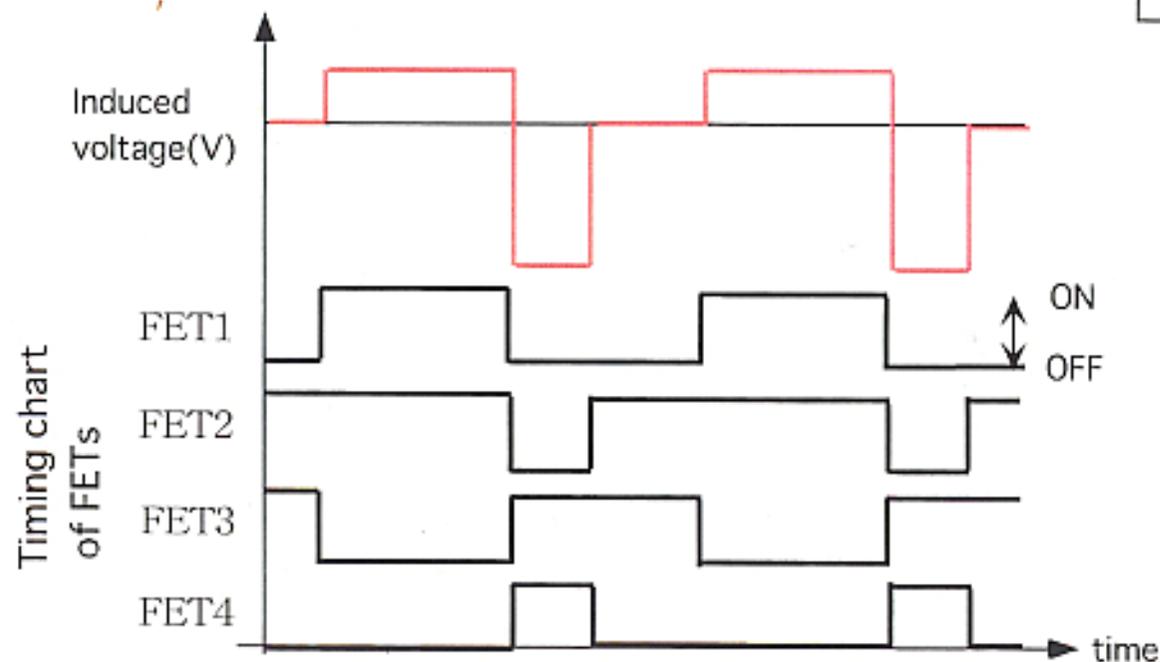
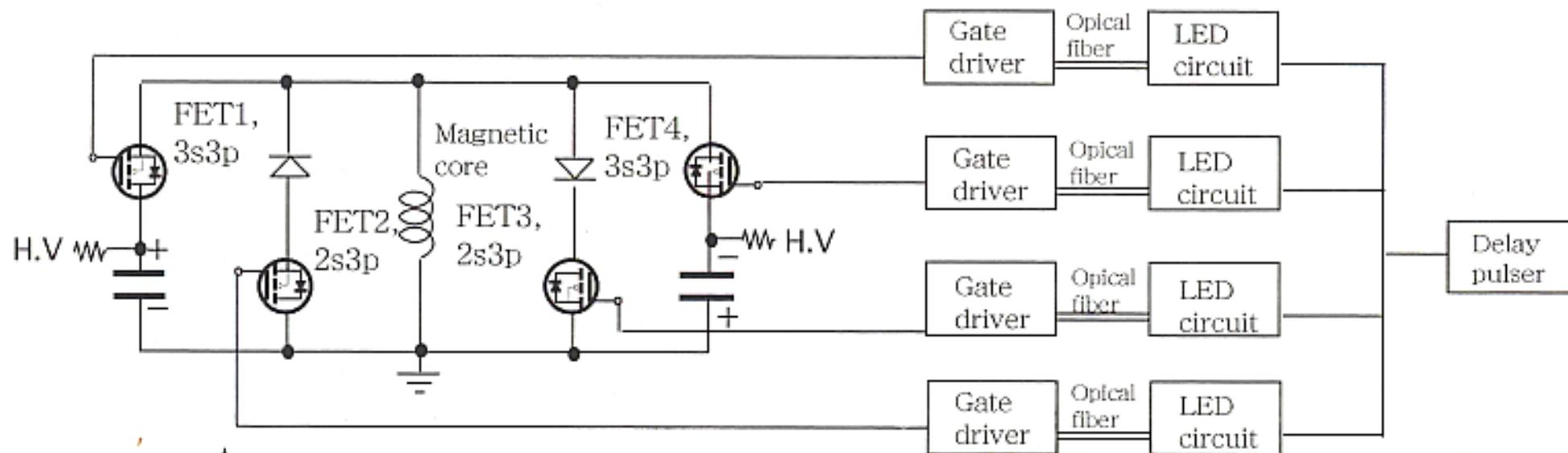
$$P(\Delta_0 B, dB/dt) = (1.74 + 5.37 \Delta_0 B) (d/\rho) (dB/dt)^{1/2} + (24.5 \Delta_0 B^2) (d^2/\rho/B_s) (dB/dt),$$

$$B_s = 1.35(T) \rho = 1.1(\mu\Omega m) \quad d = 2(\times 10\mu m) \quad \text{(Finemet)}$$

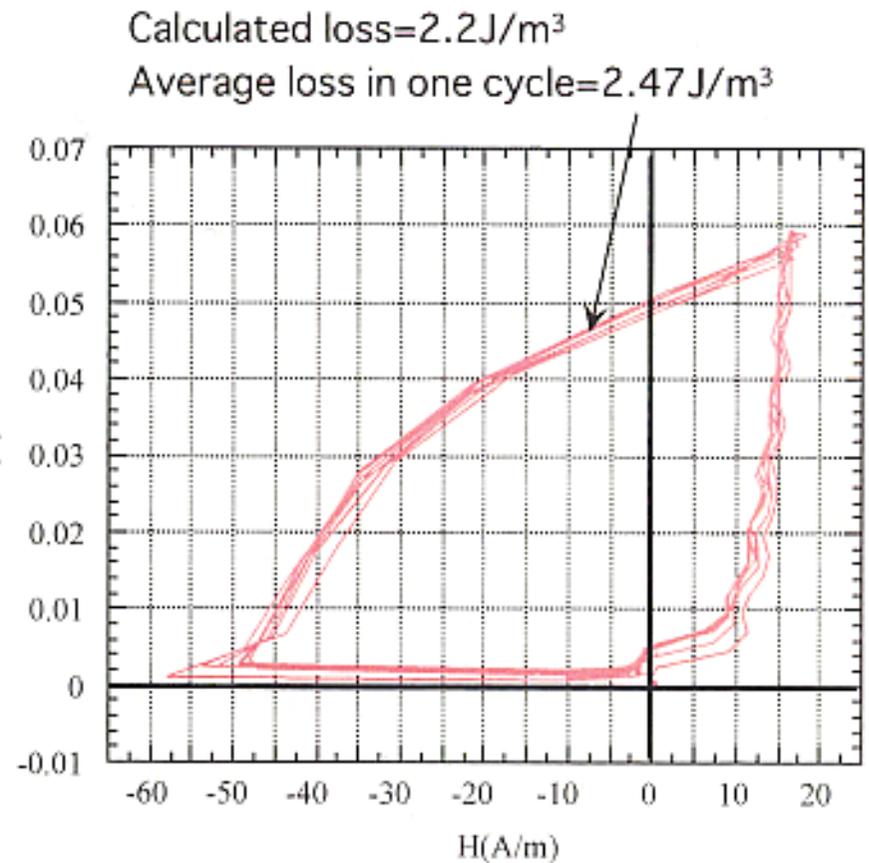
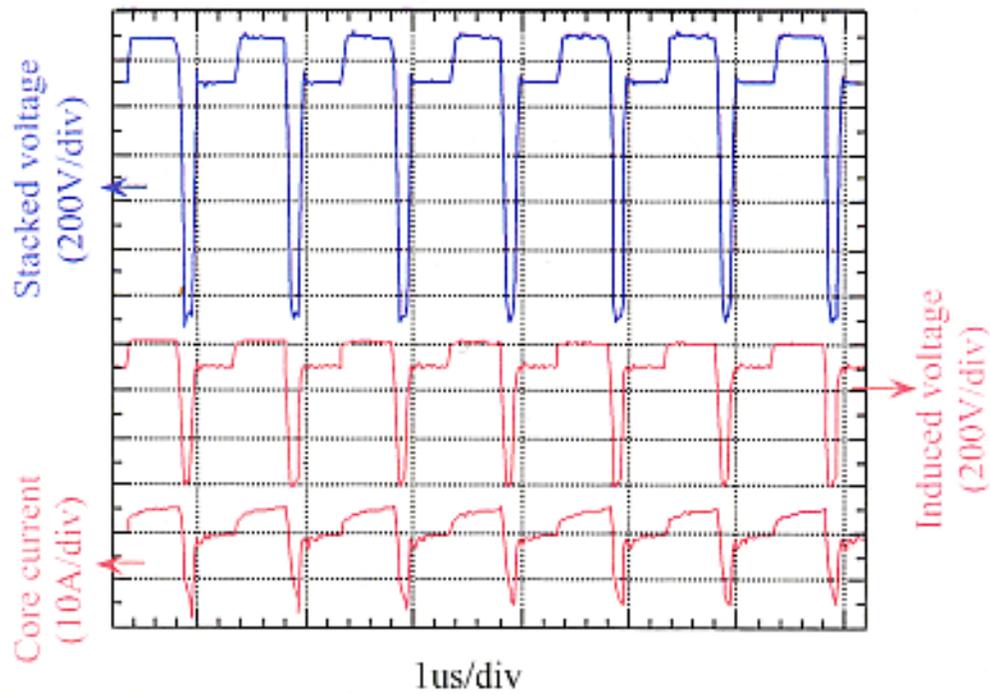
$$B_s = 0.62(T) \rho = 1.3(\mu\Omega m) \quad d = 2(\times 10\mu m) \quad \text{(Co-amorphous)}$$



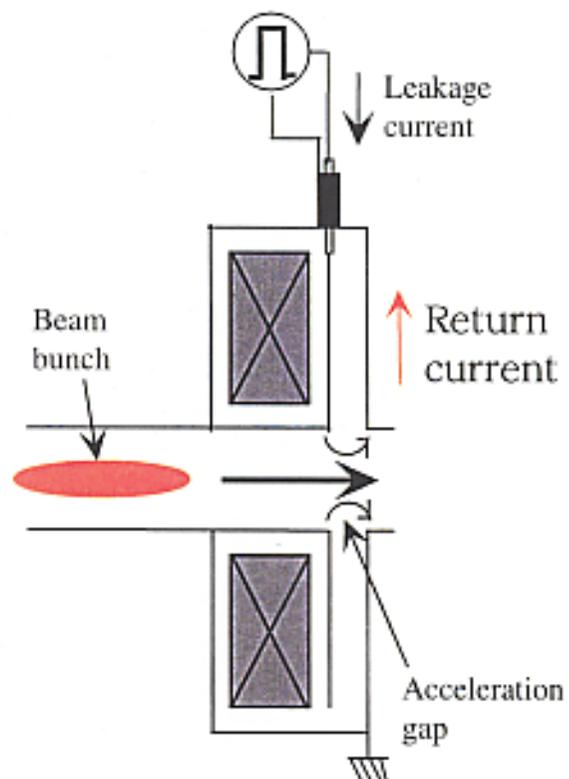
Schematic diagram of induction module



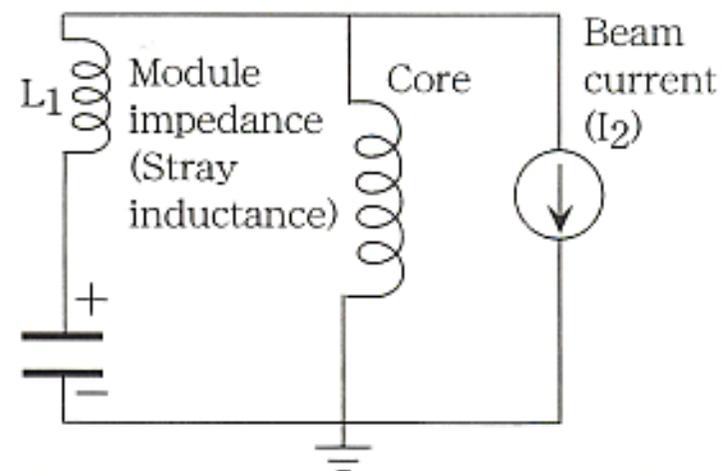
Voltage, current waveform and B-H minor loop at 1MHz



Schematic illustration of beam loading

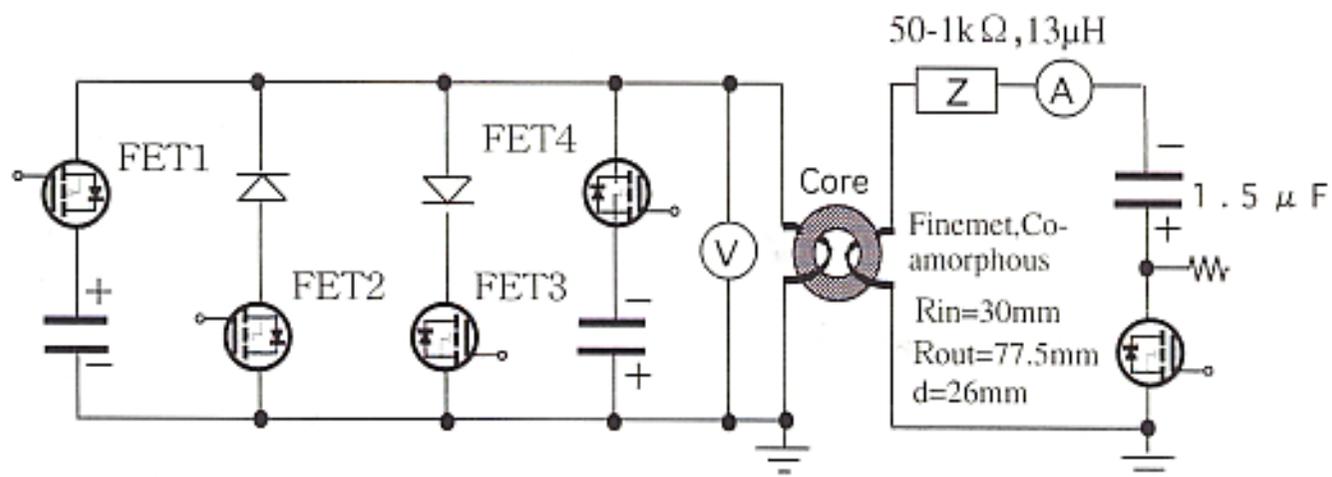


Cross section of
Induction cavity

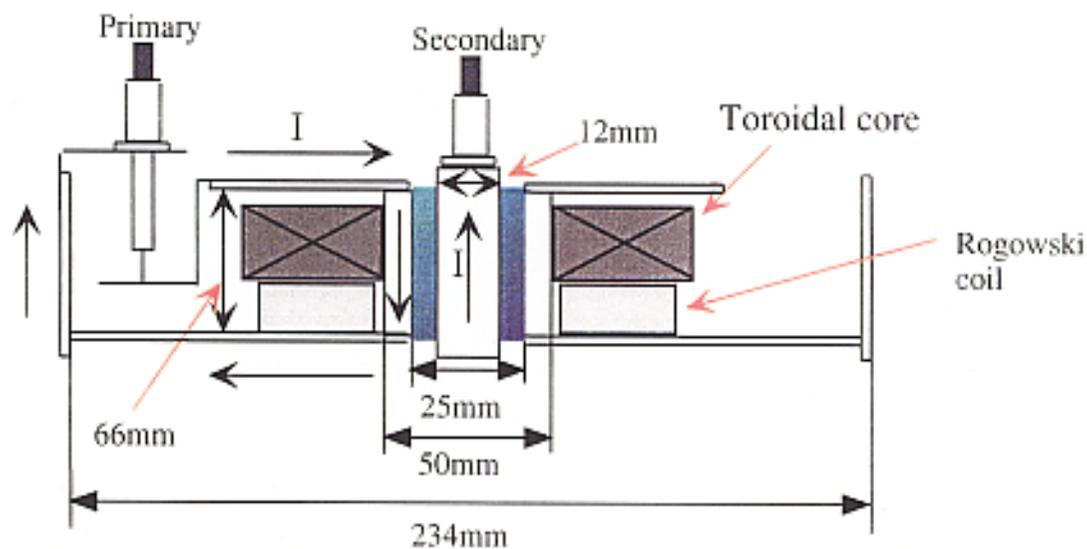


Equivalent circuit of
beam loading effect

Schematic diagram of experimental arrangement

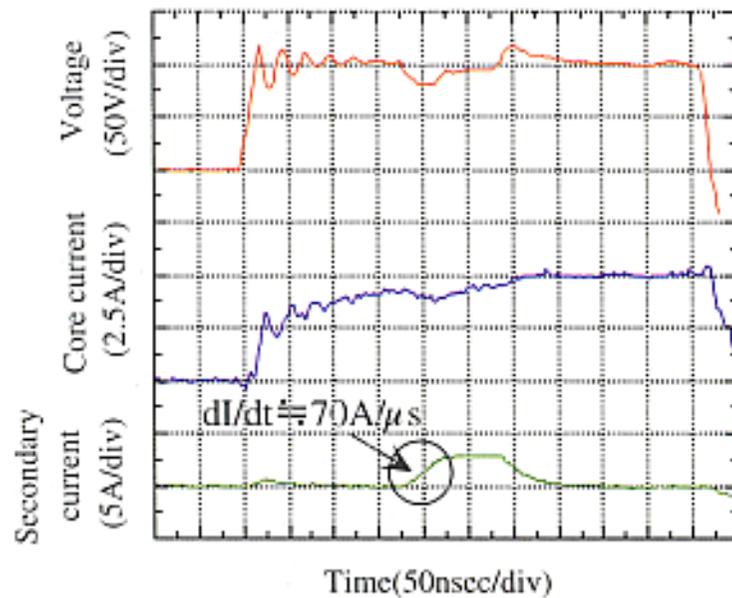


Experimental set up for beam loading experiments

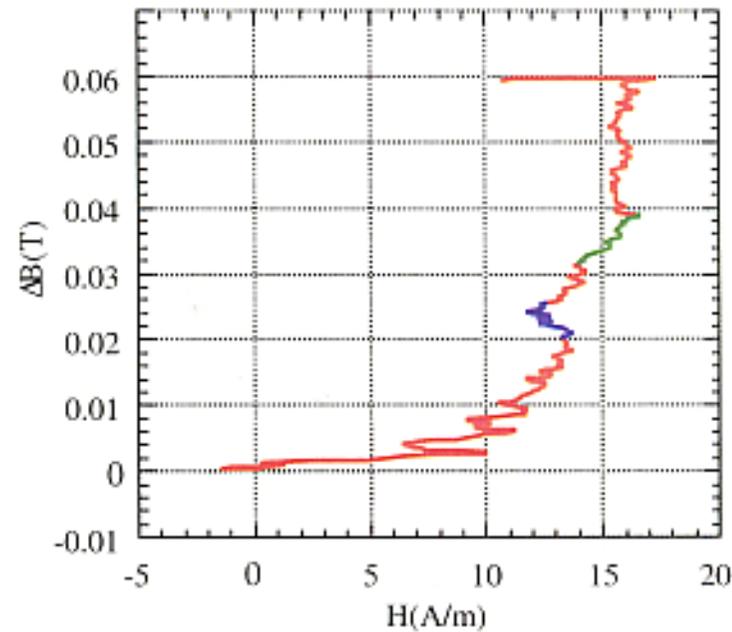


Cross section of induction element

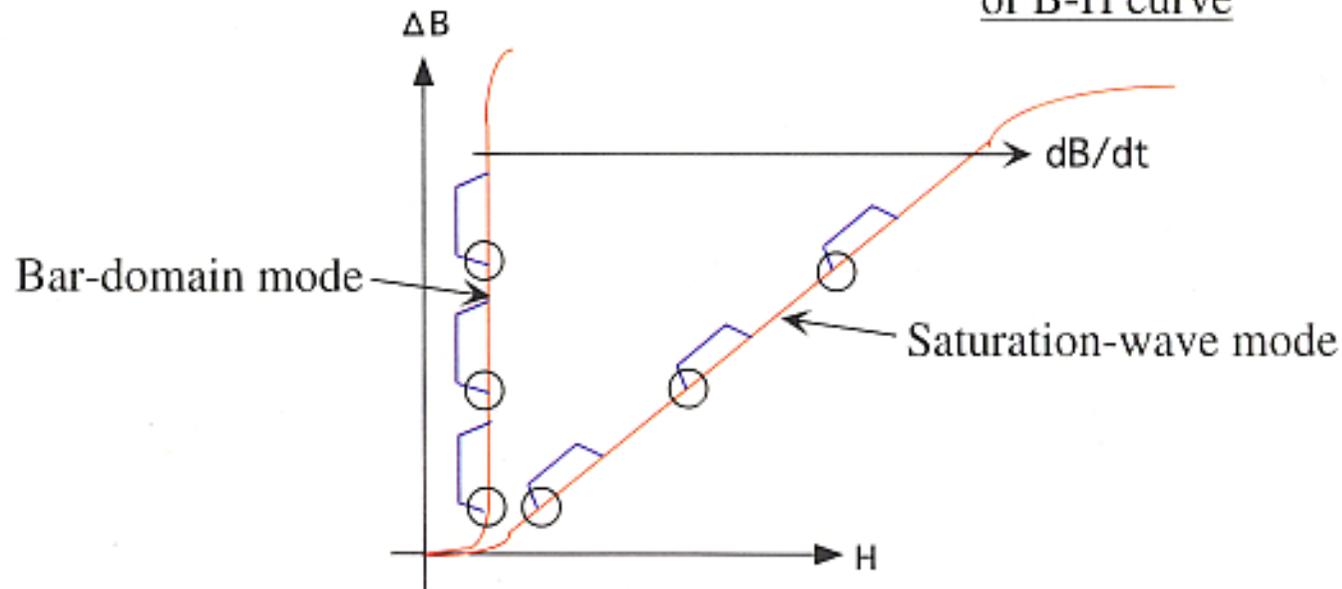
Example of Experimental result of Beam loading



Example of experimental waveform (Finemet)

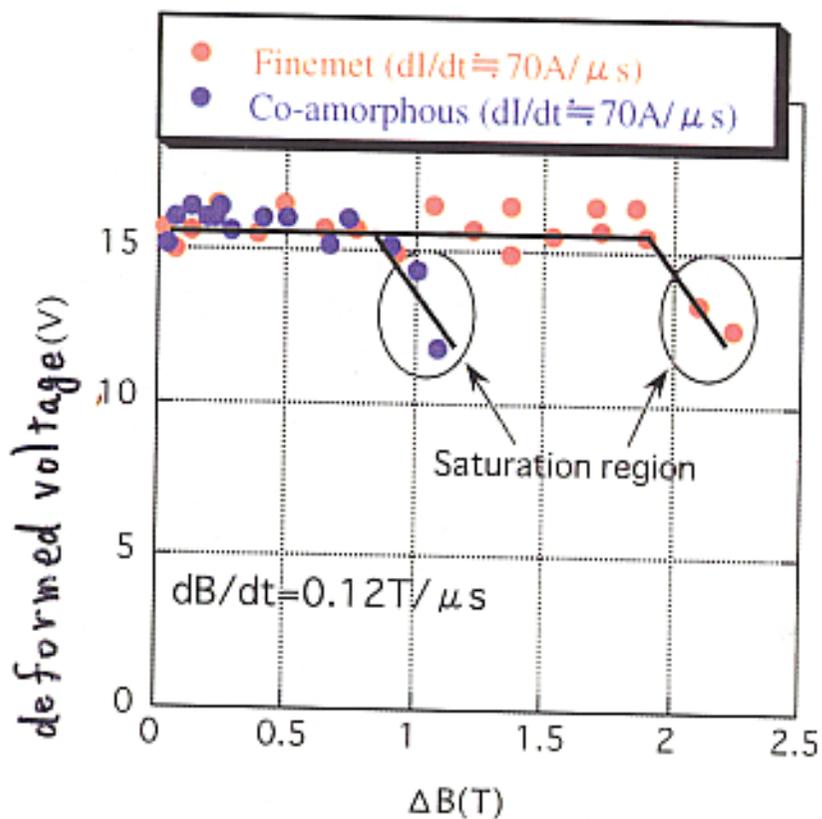


Example of core response of B-H curve



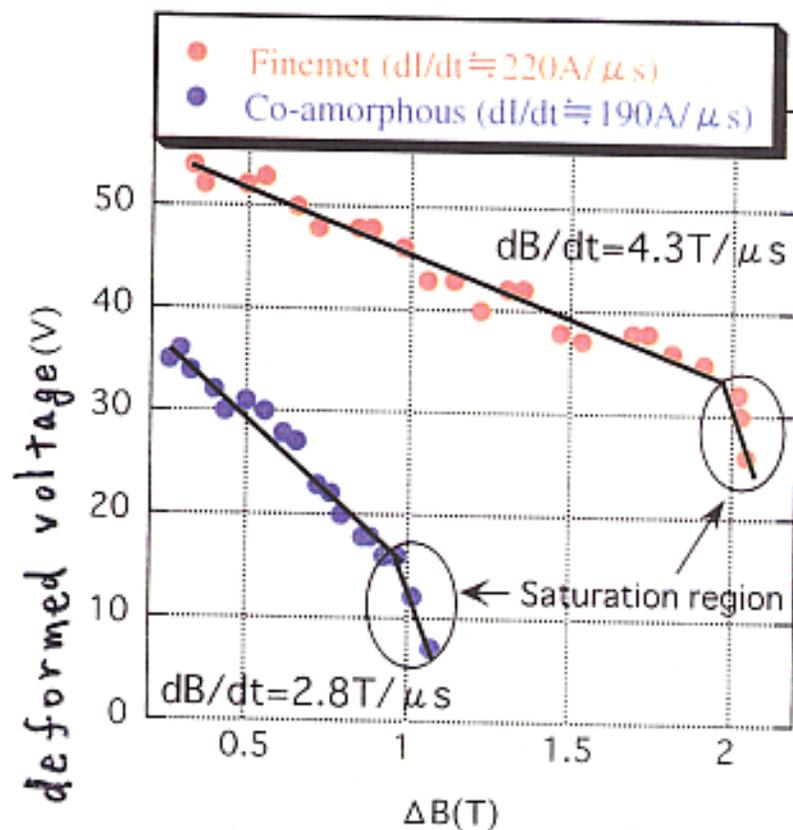
Response versus Progression of Magnetization

Bar-domain mode



Low magnetization rate

Saturation-wave mode



High magnetization rate

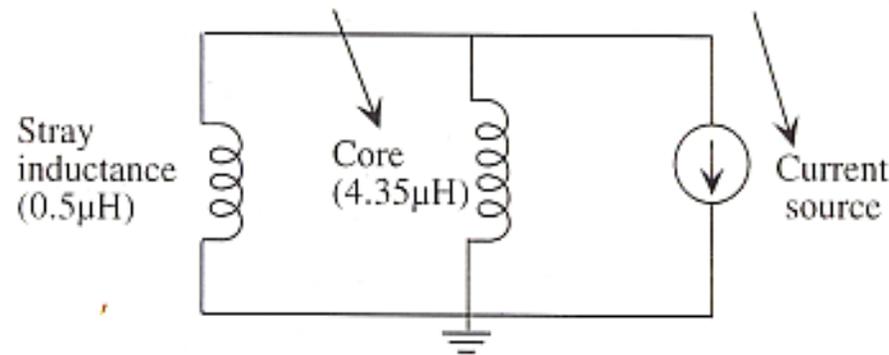
Estimation of change of the voltage in designed induction module

core size

inner diameter	10cm
outer diameter	50cm
width	5cm

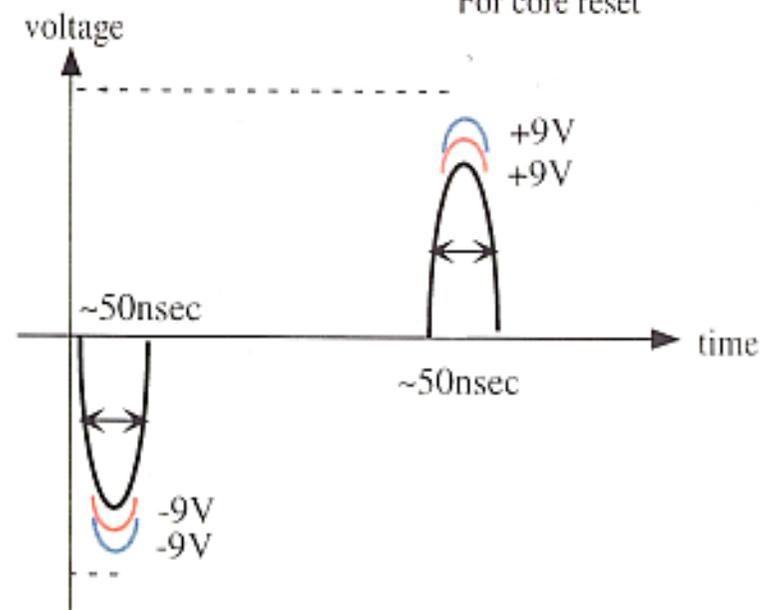
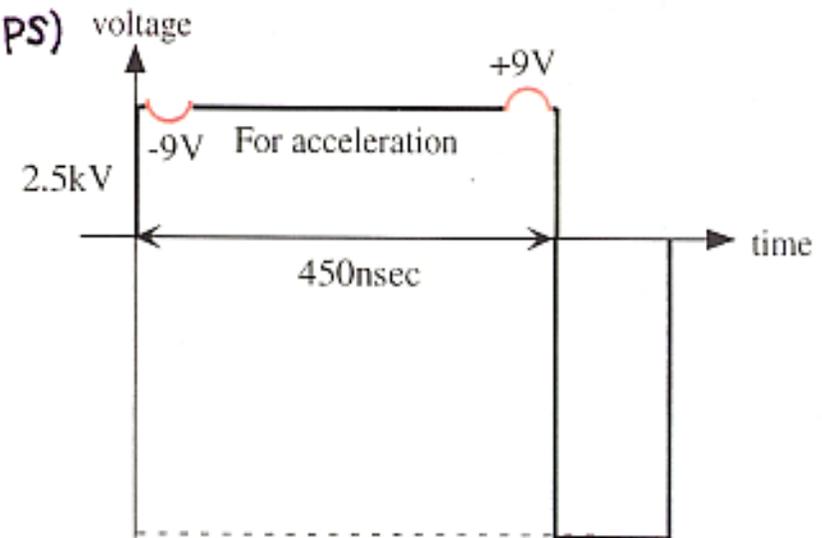
Beam parameter(12GeV-KEK-PS)

current	1A
rise time	50nsec
dI/dt	20A/ μ s



Equivalent circuit of induction module from the point of view of the secondary when using PSpice

Acceleration voltage is 2.5kV in our design. The estimated change of the voltage was about **9V**. This value is only 0.36% of the acceleration voltage.



Conclusions

- Induction modulators have been operated up-to 1MHz.
- Empirical formulae for core-losses have been obtained, which is useful for a various operating mode.
- Beam loading Effects were experimentally evaluated, which depend on non-linear effects of magnetic cores.